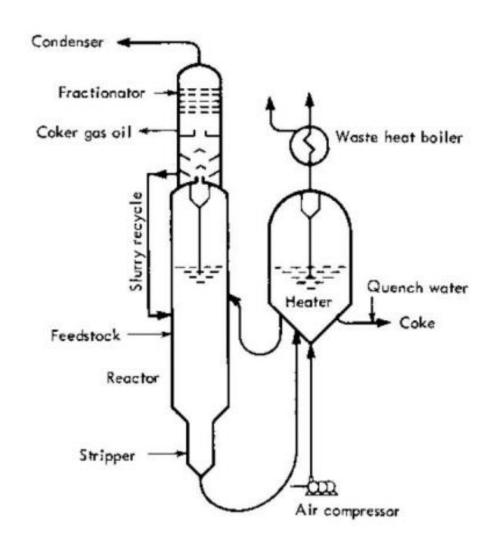
Lecture №11 Fluid Coking

Fluid coking is a continuous process that uses the fluidized solids technique to convert residua, including vacuum residua and cracked residua, to more valuable products.

This coking process allows improvement in the yield of distillates by reducing the residence time of the cracked vapors and also allows simplified handling of the coke product. Heat for the process is supplied by partial combustion of the coke, with the remaining coke being drawn as product. The new coke is deposited in a thin fresh layer (0.005 mm; 5 pm) on the outside surface of the circulating coke particle, giving an onionskin effect.

The equipment for the fluid coking process



Description of scheme

The equipment for the flu id coking process is similar to that used in flu id catalytic cracking and follows comparable design concepts except that the fluidized coke solids replace catalyst. Small particles of coke maid in the process circulate in a fluidized state between the vessels and are the heat transfer medium; thus the process requires no high temperature preheat furnace.

Fluid coking uses two vessels—a reactor and a burner. Coke particles are circulated between these to transfer heat (generated by burning a portion of the coke) to the reactor The reactor holds a bed of fluidized coke particles, and steam is introduced at the bottom of the reactor to fluidize the bed. The feed coming from the bottom of a vacuum tower at, for example, 260–370°C (500–700°F), is injected directly into the reactor. The temperature in the coking vessel ranges from 480°Cto 565°C (900–1050°F), with short residence times on the order of 15–30 s, and the pressure is substantially atmospheric, so the incoming feed is partly vaporized and partly deposited on the fluidized coke particles. The material on the particle surface then cracks and vaporizes, leaving a residue that dries to form coke. The vapor products pass through cyclones that remove most of the entrained coke.

Vapor products leave the bed and pass through cyclones, which are necessary for removal of the entrained coke. The cyclones discharge the vapor into the bottom of a scrubber, any coke dust remaining after passage through the cyclones is scrubbed out with a pump around stream, and the products are cooled to condense the heavy tar. The resulting slurry is recycled to the reactor. The scrubber overhead vapors are sent to a fractionator, where they are separated into wet gas, naphtha, and various gas oil fractions. The wet gas is compressed and further fractionated into the desired components.

In the reactor the coke particles flow down through the vessel into the stripping zone. The stripped coke then flows down a standpipe and through a slide valve that controls the reactor bed level. A riser carries the cold coke to the burner. Air is introduced to the burner to burn part of the coke to provide reactor heat. The hot coke from the burner flows down a standpipe through a slide valve that controls coke flow and thus the reactor bed temperature. A riser carries the hot coke to the top of the reactor bed. Combustion products from the burner bed pass through two stages of cyclones to recover coke fines and return them to the burner bed.

Coke is withdrawn from the burner to keep the solids inventory constant. To aid in keeping the coke from becoming too coarse, large particles are selectively removed as product in a quench elutriator drum, and coke fines are returned to the burner. The product coke is quenched with water in the quench elutriator drum, and pneumatically transported to storage. A simple jet attrition system in the reactor provides additional seed coke to maintain a constant particle size within the system.

Due to the higher thermal cracking severity used in fluid coking compared to delayed coking, the products are somewhat more olefinic than the products from delayed coking. In general, products from both coking processes are handled for upgrading in a comparable manner.

Coke, being a product of the process, must be withdrawn from the system to keep the solids inventory from increasing. The net coke produced is removed from the burner bed through a quench elutriator drum, where water is added for cooling and cooled coke is withdrawn and sent to storage. During the course of the coking reaction the particles tend to grow in size. The size of the coke particles remaining in the system is controlled by a grinding system within the reactor.

The coke product from the fluidized process is a laminated sphere with an average particle size of 0.17–0.22 mm (170–220 μ m), readily handled by fluid transport techniques. It is much harder and denser than delayed coke and in general is not as desirable for manufacturing formed products.

The yields of products are determined by the feed properties, the temperature of the fluid bed, and the residence time in the bed. The lower limit on operating temperature is set by the behavior of the fluidized coke particles. If the conversion to coke and light ends is too slow, the coke particles agglomerate in the reactor, a condition known as *bogging*. The use of a fluidized bed reduces the residence time of the vapor-phase products in comparison to delayed coking, which in turn reduces cracking reactions. The yield of coke is thereby reduced, and the yield of gas oil and olefins is increased. An increase of 5°C (9°F) in the operating temperature of the fluidized bed reactor typically increases gas yield by 1wt% and naphtha by about 1wt%.

The disadvantage of burning the coke to generate process heat is that sulfur from the coke is liberated as sulfur dioxide (SO_2). The gas stream from the coke burner also contains carbon monoxide (CO_2), carbon dioxide (CO_2), and nitrogen (N_2). An alternative approach is to use a coke gasifier to convert the carbonaceous solids to a mixture of CO_2 , and hydrogen (H_2).